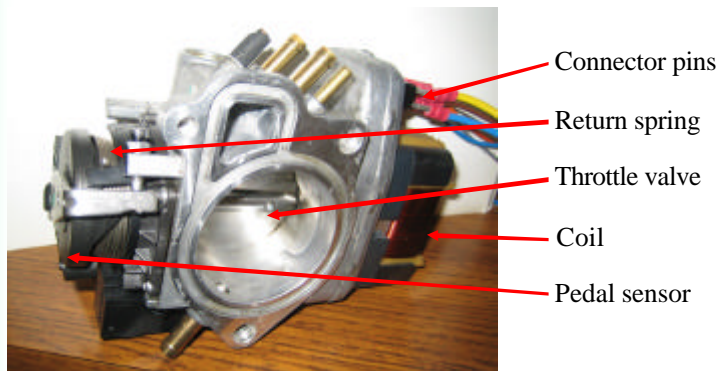


Hardware in the loop for Electronic Throttle System Identification and Control

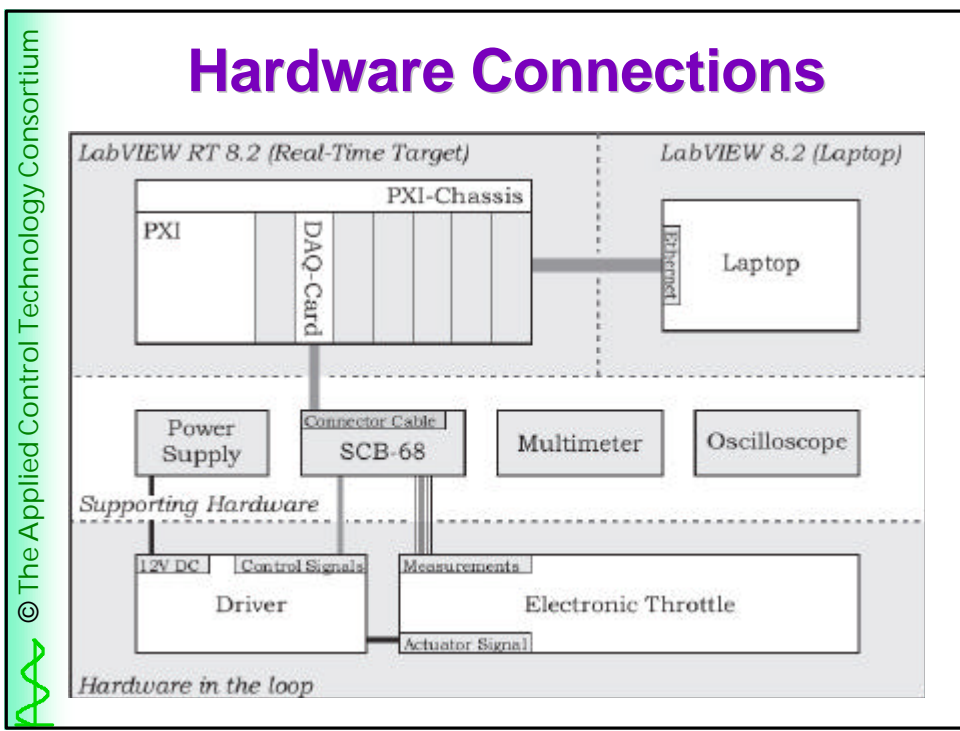
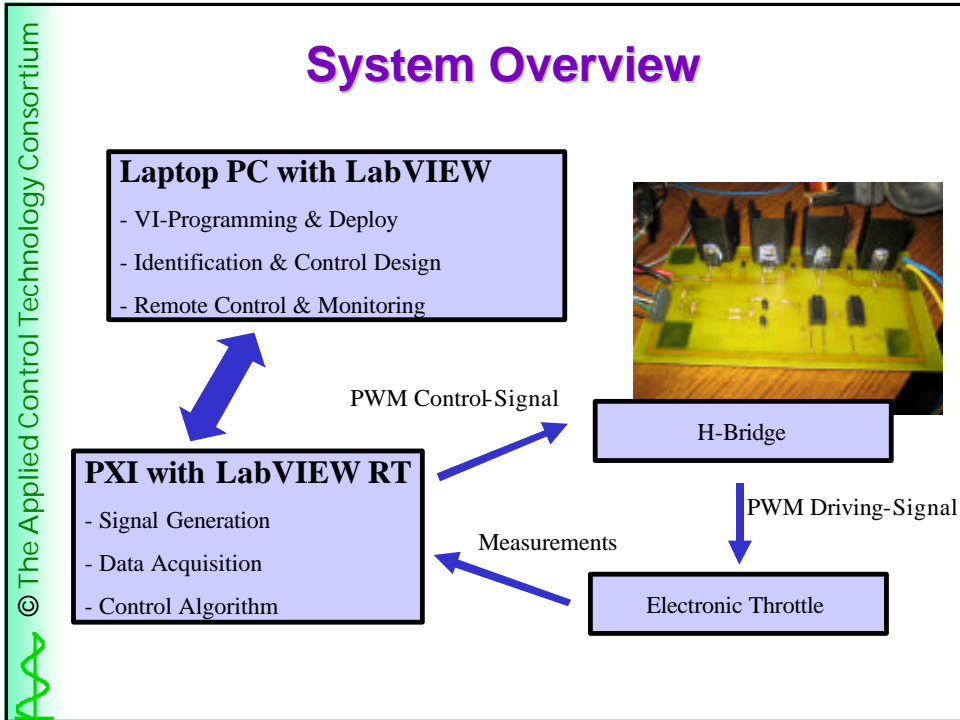
Dr. Arek Dutka
ACTC

Electronic Throttle Body

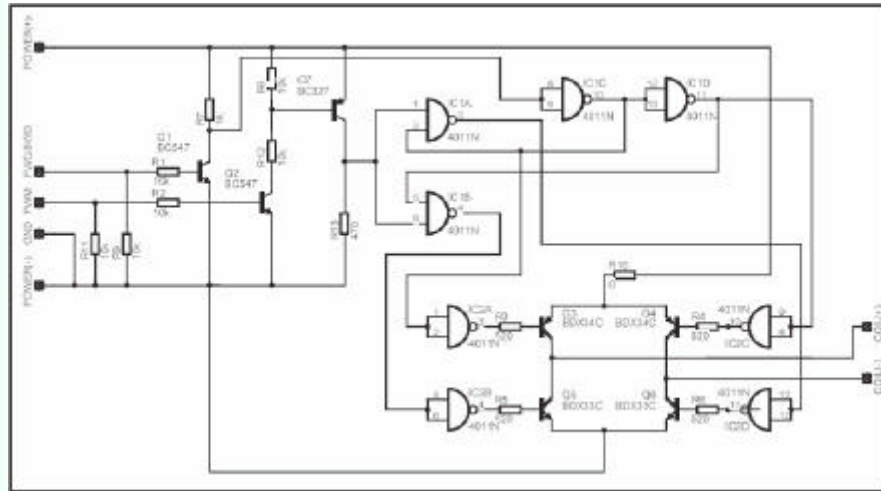


Pedal and Throttle positions decoupling results in:

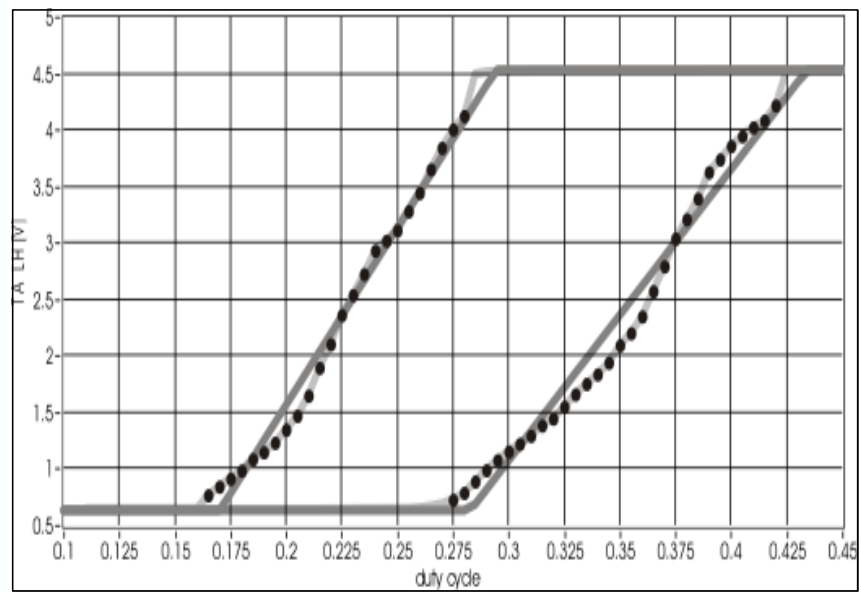
- Lower fuel consumption
- Better engine torque control
- Different engine response available (normal, snow, mountains)



Driver (Power Amplifier)

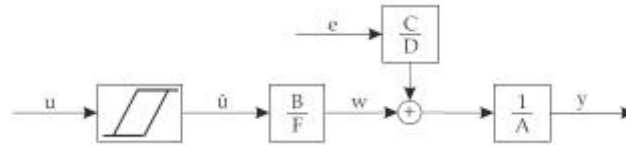


Steady State Characteristic



System model structure

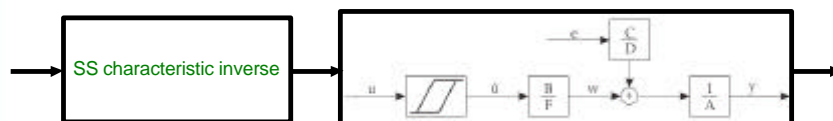
- The following Hammerstein model structure will be used for modelling



- Results will be compared with the pure linear model
- The above model structure suggests that the steady-state characteristic is a part of the system located before the linear dynamics

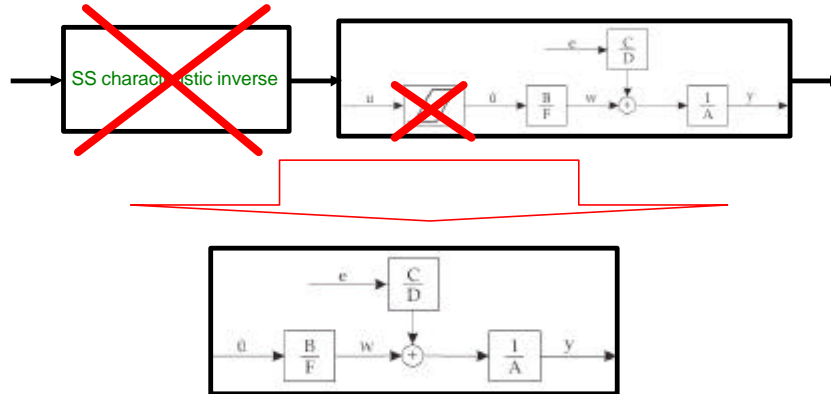
System model structure

- The assumption may not be in line with reality
 - Steady-state response and dynamics may not be separable
 - Dynamics may be non-linear
- Let's assume that our assumptions are sufficiently accurate
 - Remove the steady-state behaviour by using a pseudo-inverse of the steady-state characteristic



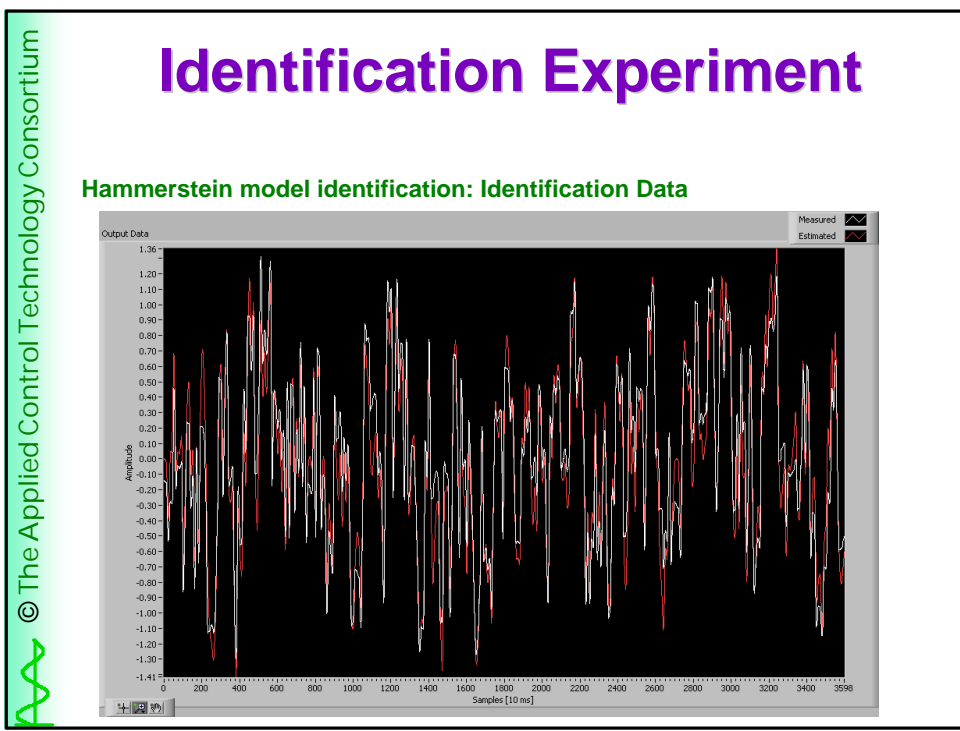
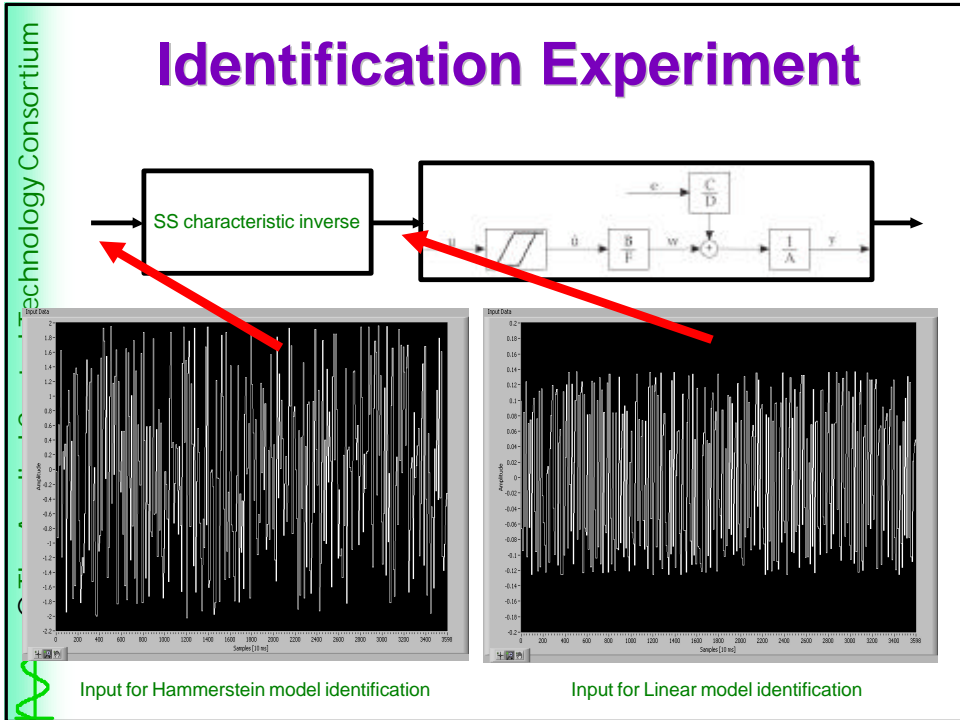
System model structure

- Assuming that the static non-linearity is cancelled out by the pseudo-inverse the remaining model of the system is linear:



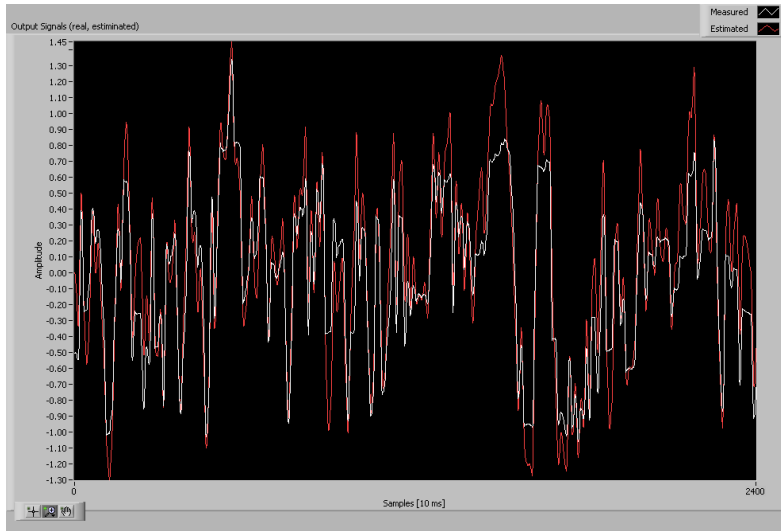
Identification Experiment

- Inverse of the input characteristic scales the input to the ‘virtual linear system’ with the similar input-output range
 - This range is about 0.63 ... 4.53 [V]
- The random signal is generated and passed through the inverse of the steady-state characteristic
 - Signal that is obtained on the SS Characteristic output is a Duty Cycle signal that is sent to the power amplifier and the Electronic Throttle’s coil



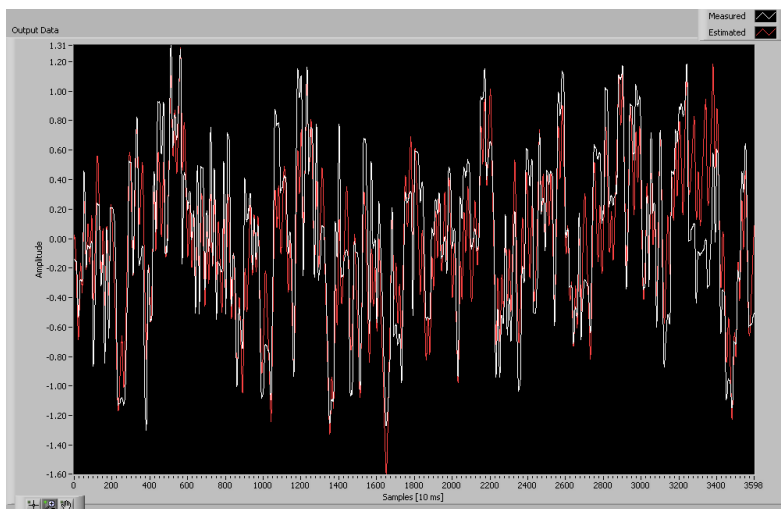
Identification Experiment

Hammerstein model identification: Validation Data



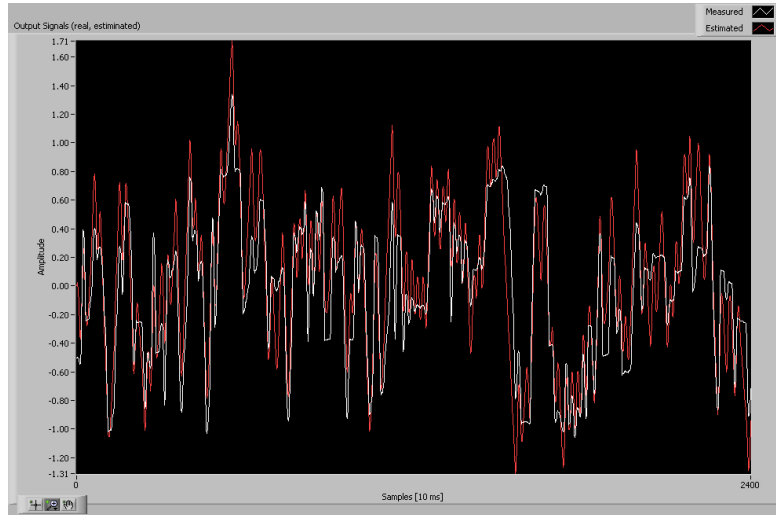
Identification Experiment

Linear model identification: Identification Data

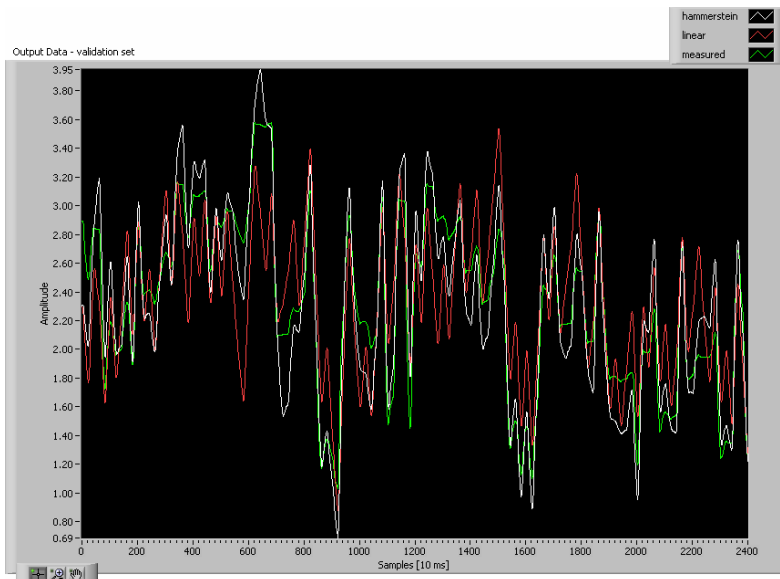


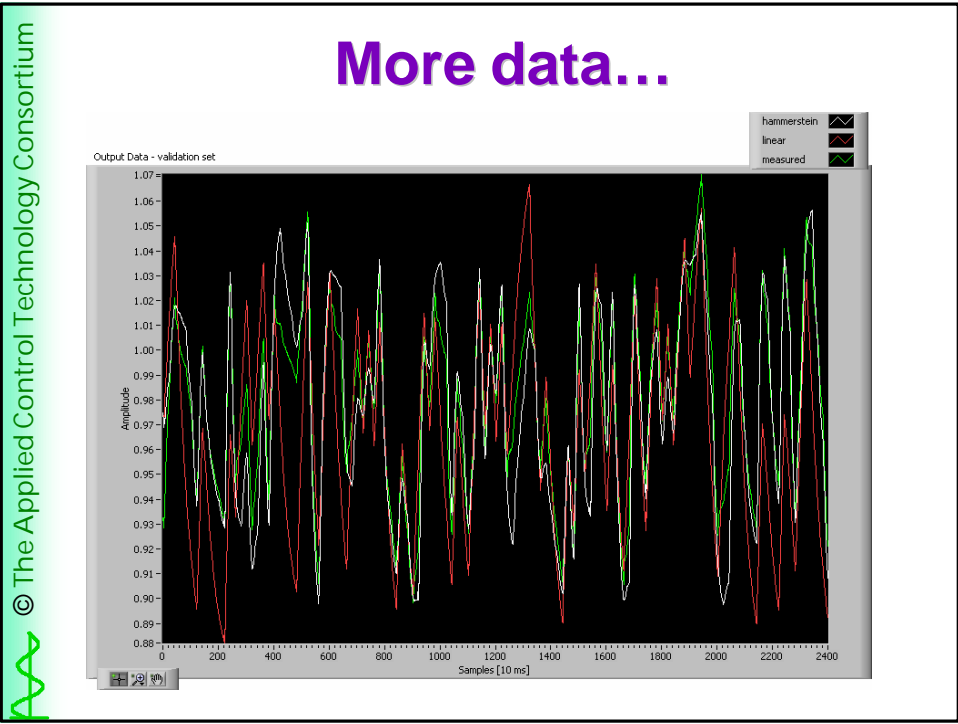
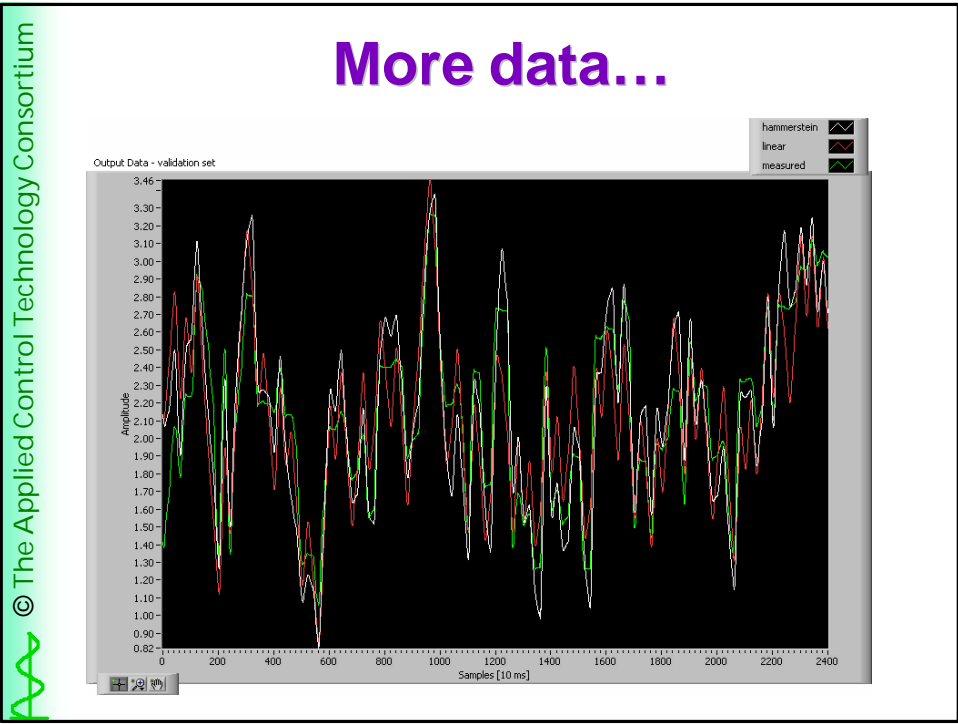
Identification Experiment

Linear model identification: Validation Data

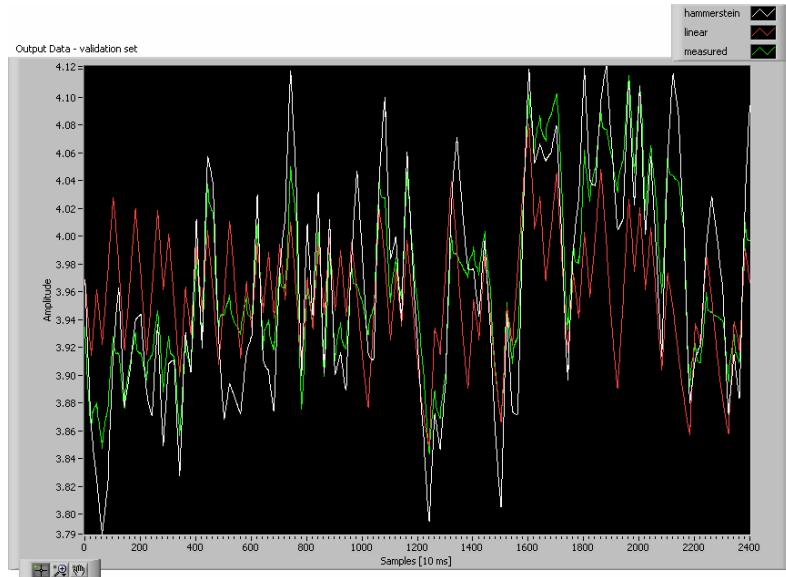


More data...

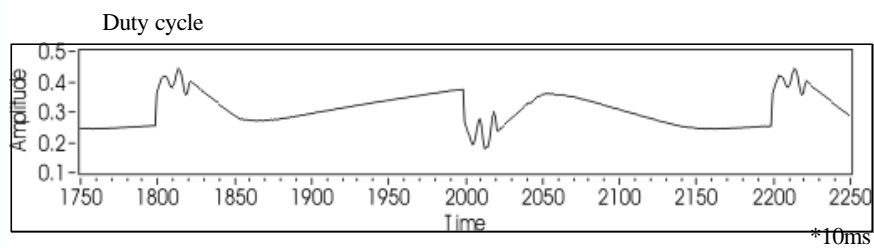
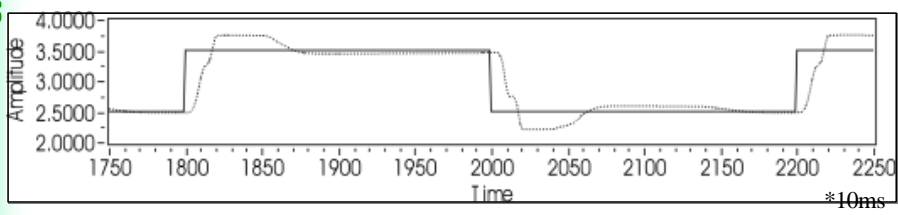


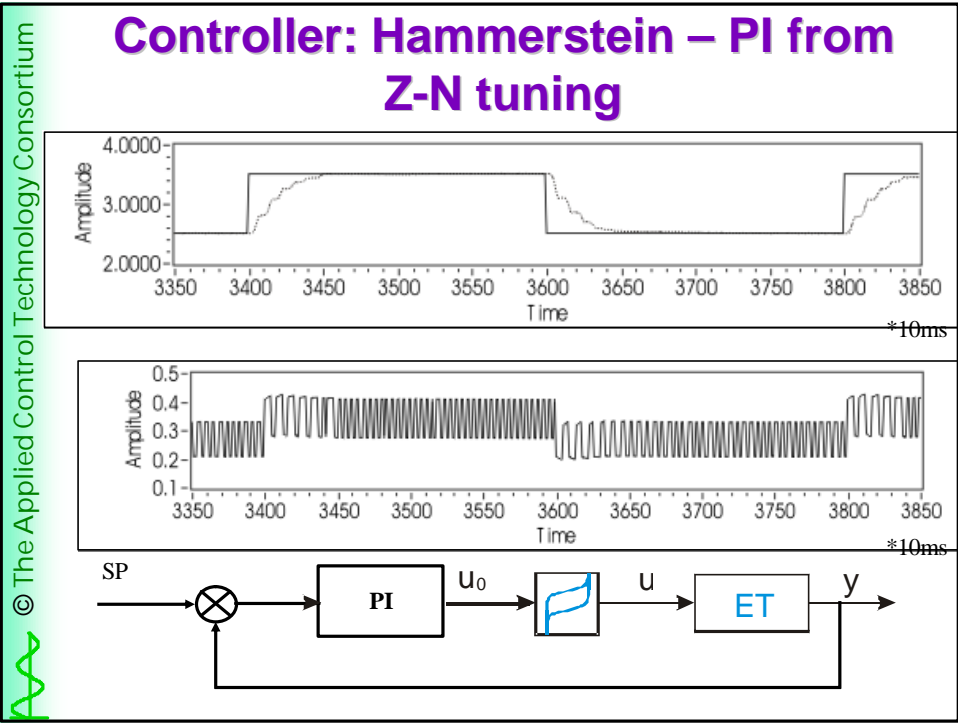
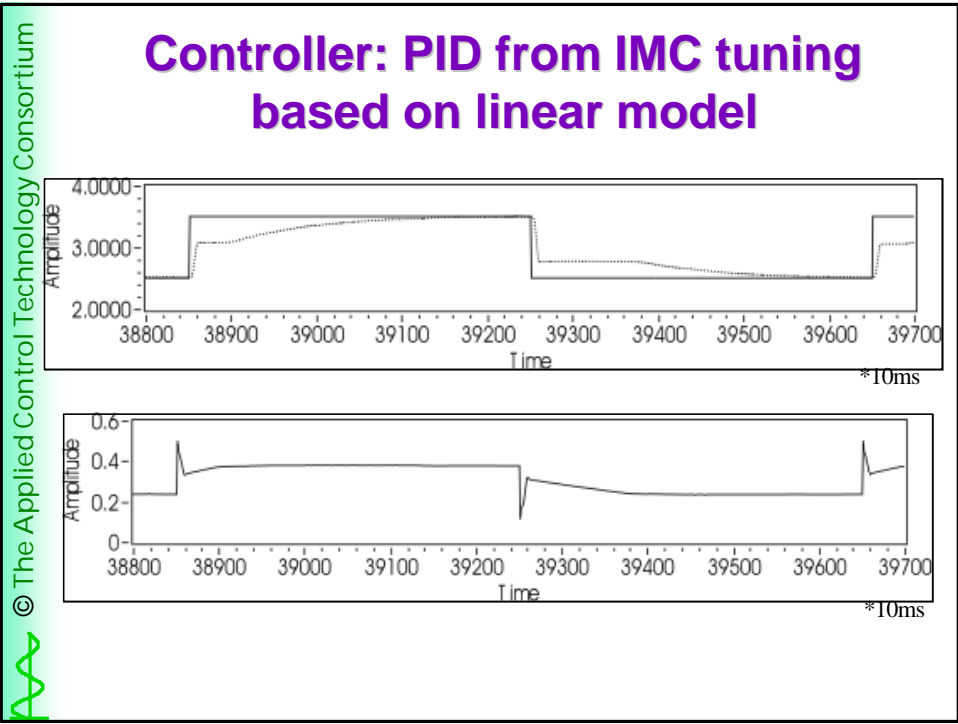


More data...

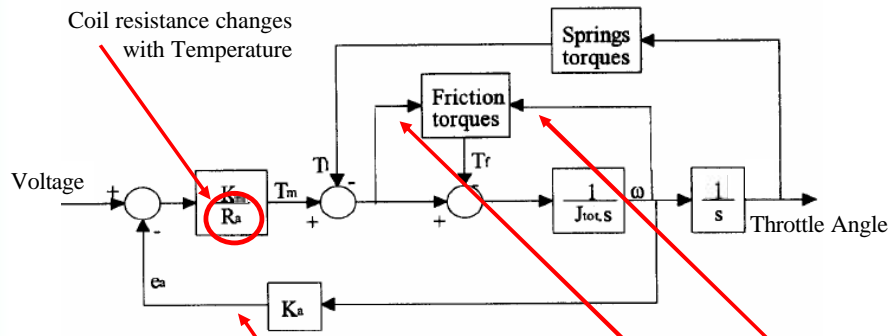


Controller: Hand-tuned - PID





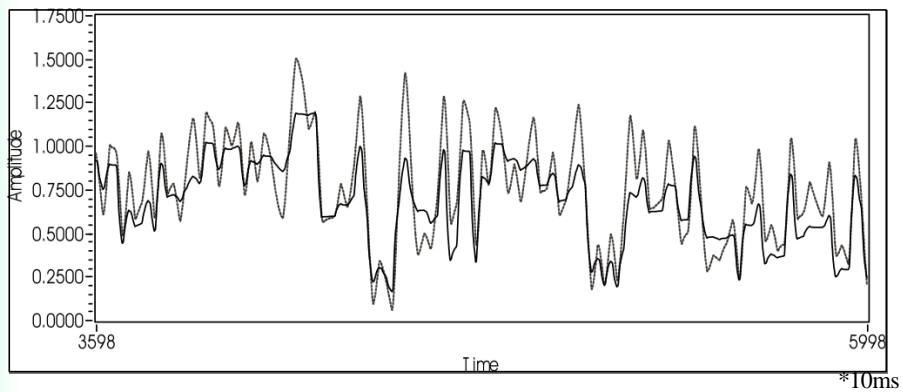
Physical Model



- Neglected electric dynamics
- Back electromotive force
- Spring torque
- Friction torques (stiction/Coulomb friction)

R.Scattolini et al.: „Modeling and Identification of an electromechanical Internal Combustion Engine Throttle Body. Control Eng. Practice, Vol. 5, No.9, pp. 1253-1259, 1997.

Physical Model Identification Result



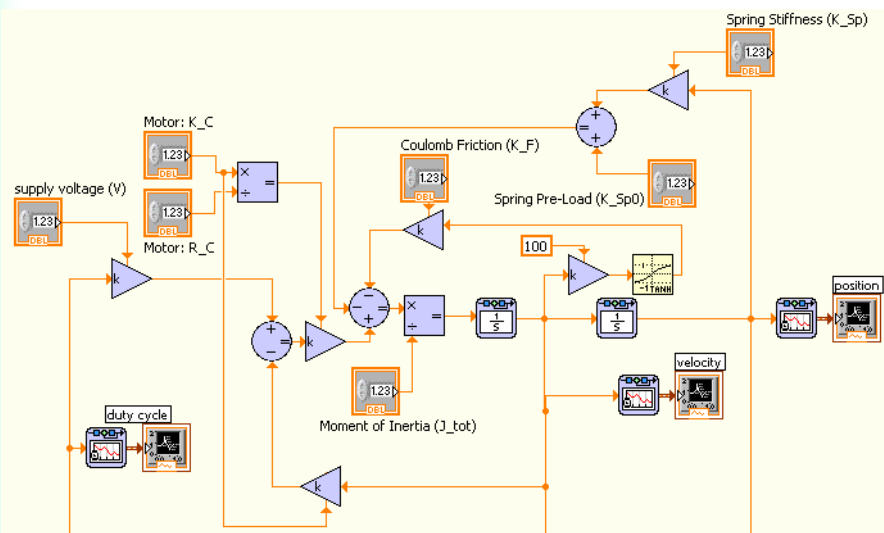
Mean squared error of scaled data:
0.057

- Note: Hammerstein model was 0.026

Problems with EKF identification

- The discretisation of the system with discontinuities causes numerical problems (e.g. Coulomb friction – substituted by $\tanh()$)
- The model contains 6 unknown parameters – simultaneous identification depends on initial conditions
- Overall, poor knowledge of the initial system parameters which caused problems
- Unmodelled nonlinearities, observable in the steady state characteristic, might affect these results

Simulation model

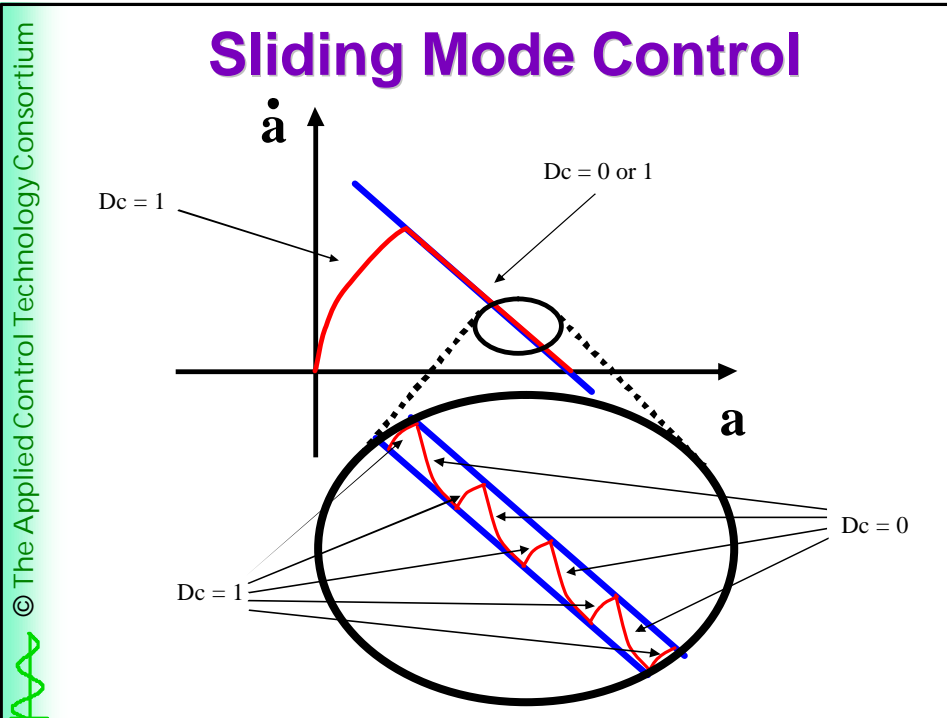


Alternative Control Technique

- PID control performance was not good enough: poor speed of response
 - This was the case for PID controller designed based on:
 - Manual tuning
 - Linear model based tuning
 - Non-Linear model based tuning
- The best result was obtained for Hammerstein model
 - But with significant amount of control activity

Alternative Control Technique

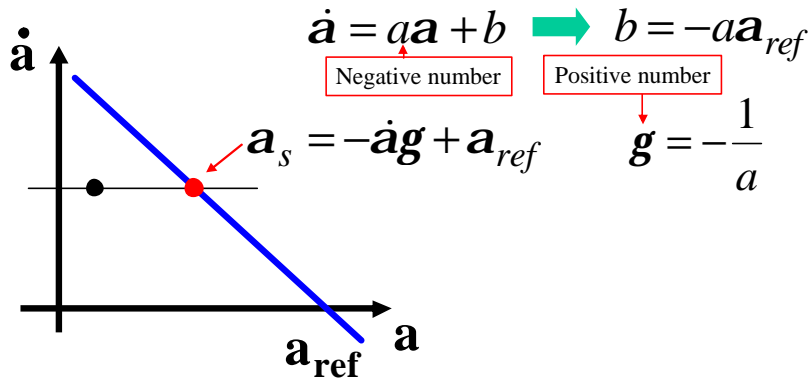
- Since the throttle is controlled through PWM modulation, the control signal is discontinuous and fast-switching
- This suggests that Sliding Mode control technique might be considered
- We'll use system simulation to investigate properties of that control technique



- Sliding Mode Control**
- The approach used here is by far simpler than the formal Sliding Mode Control technique
 - Based on relay control
 - Depending on the current being on/off the throttle angle rate will increase or decrease
 - The sliding manifold will need to be adjusted for these rates to give stable response
 - The controller will be very simple with only 1 tuning parameter
- © The Applied Control Technology Consortium

Sliding Mode Control

- We'll use the model identified with the EKF

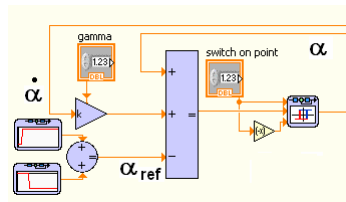


$$a - a_s = \dot{a} g - a_{ref} + a < 0$$

Need to increase speed (increase control)

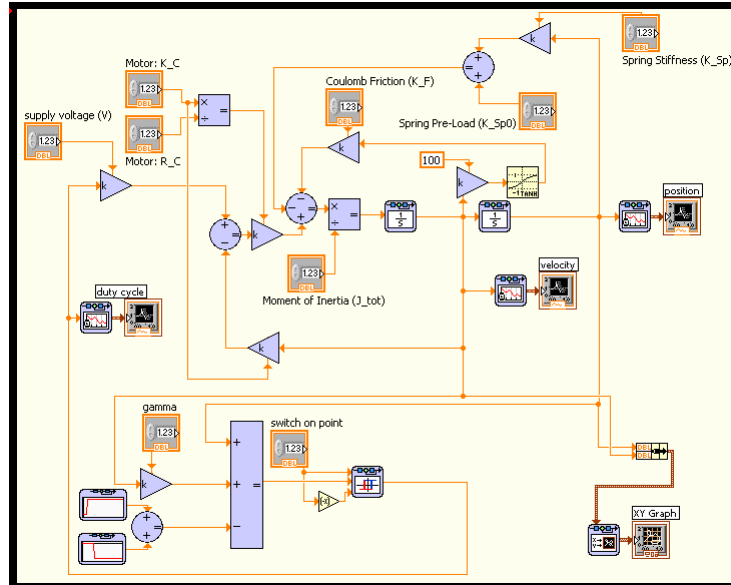
Sliding Mode Control

- The controller is implemented below:

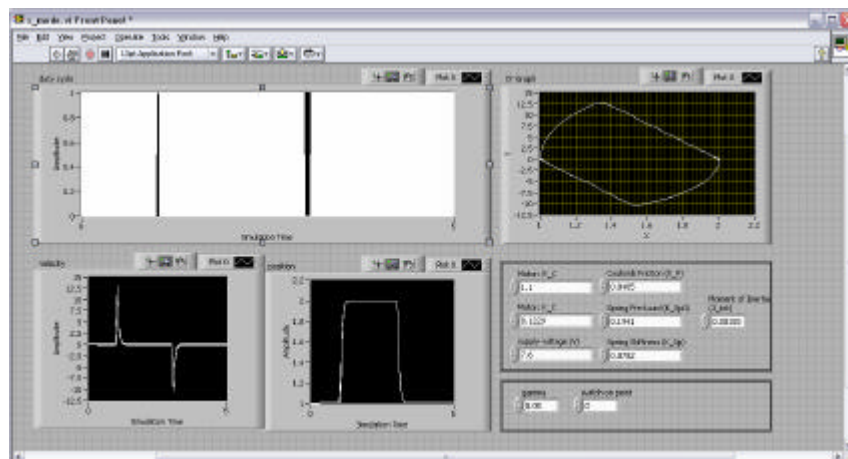


- The relay detects if control needs to be set to max. value or minimum value (0)
 - It is also possible to introduce a hysteresis to reduce switching frequency

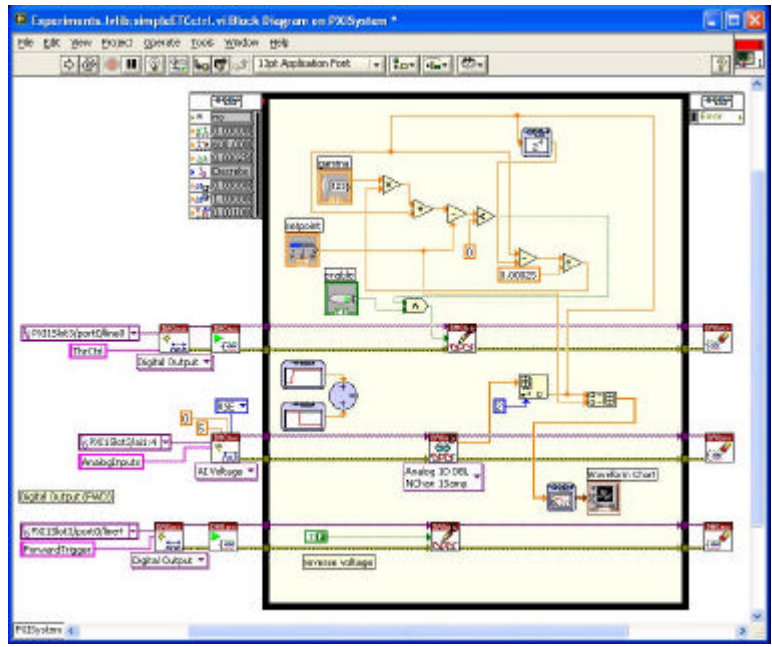
System simulation: diagram



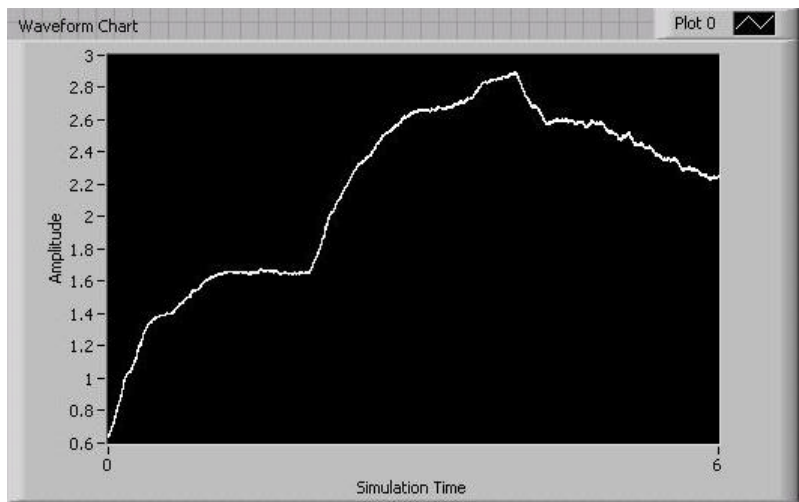
System simulation: front panel



Hardware results

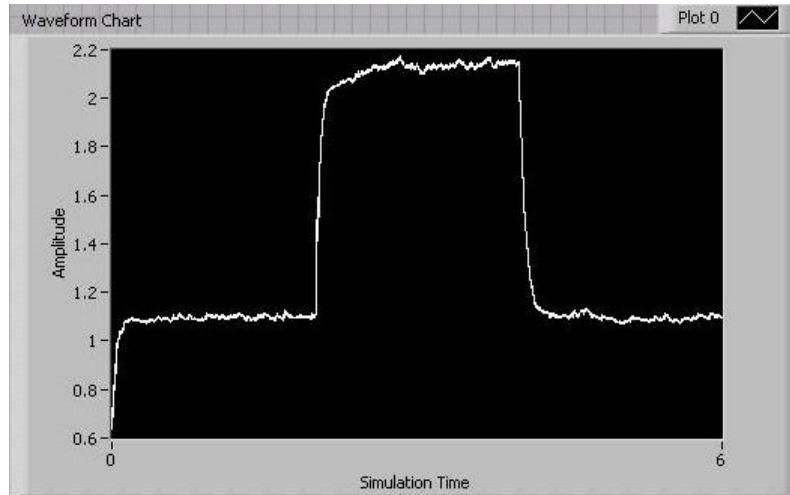


Hardware results



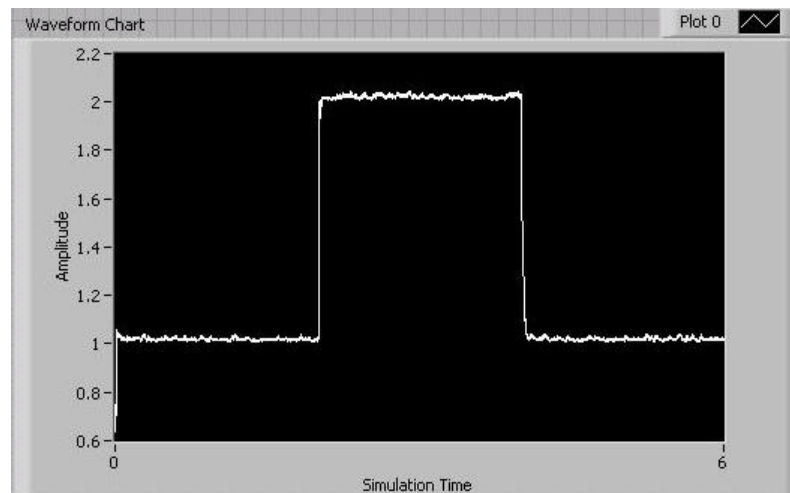
Gamma = 0.5

Hardware results



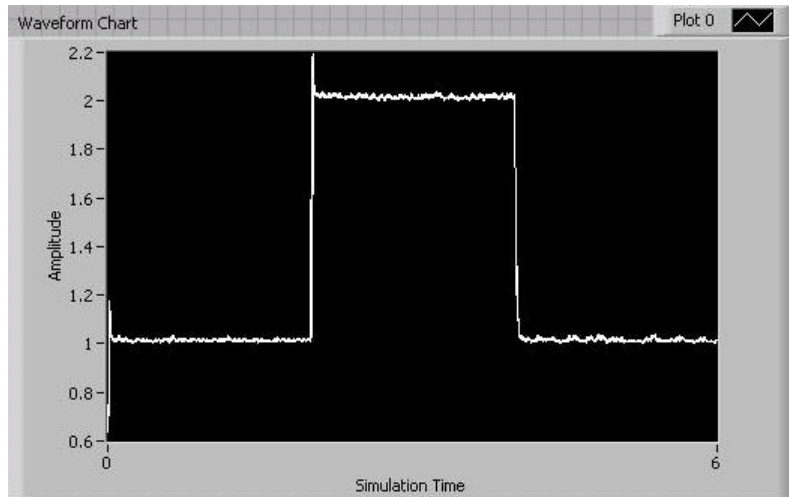
Gamma = 0.05

Hardware results



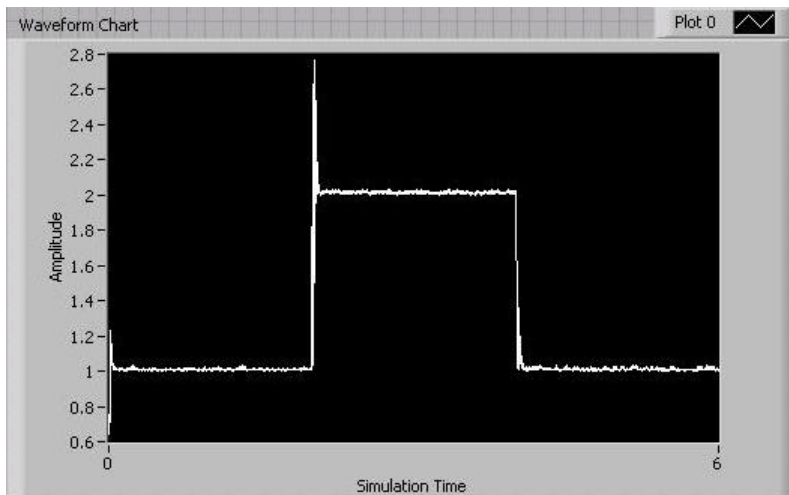
Gamma = 0.01

Hardware results



Gamma = 0.008

Hardware results



Gamma = 0.005

Hardware results



Gamma = 0.0005

Thank you!